The propagation and seismicity of dyke injection, new experimental evidence.

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Key points (3x80 char):

- Hybrid-analogue rock deformation experiments using Plexiglas/basalt.
- AE monitoring the formation of tensile fractures, and subsequent viscous fluid flow.
- Fracturing and fluid movement are characterized by different frequency spectra.
Abstract [150 words]

To reach the surface, dykes must overcome the inherent tensile strength of the country rock. As they do they generate swarms of seismic signals, frequently used for forecasting. In this study we pressurize and inject molten acrylic into an encapsulating host rocks of 1) Etna basalt and 2) Comiso limestone; at 30 MPa of confining pressure. Fracture was achieved at 12 MPa for Etna basalt, 7.2 MPa for Comiso limestone. The generation of radial fractures was accompanied by acoustic emissions (AE) at a dominant frequency of 600 kHz. During “magma” movement in the dykes, AE events of approximately 150 kHz dominant frequency were recorded. We interpret our data using AE location and dominant frequency analysis, concluding that the seismicity associated with magma transport in dykes peaks during initial dyke creation but remains significant as long as magma movement continues. These results have important implications for seismic monitoring of active volcanoes.

Index terms:

4316 Physical modeling (0466, 0545, 0798, 1622, 1847, 1952, 3355, 3367)
8419 Volcano monitoring (4302, 7280)
8488 Volcanic hazards and risks (4302, 4328, 4333)
8434 Magma migration and fragmentation
7280 Volcano seismology (4302, 8419)

Keywords:

Volcanic Basement, Dyke formation, Basalt, Limestone, Deformation, HPT Experiments
1. Introduction

Seismic signals are a key monitoring tool for assessing the unrest and eruptive state of active volcanoes [e.g., McNutt, 1996; Chouet, 2003]. A wide range of seismicity is observed, ranging from volcano-tectonic events (e.g., fracturing of rocks) to low frequency harmonic tremor thought to be driven by fluid migration within the fractured edifice [e.g., Chouet, 2003]. The analysis of such seismic datasets includes tools such as 1) 3D location, 2) event rate acceleration in order to forecast an edifice [e.g., Kilburn, 2012] or magma failure time [Lavallée et al., 2008], and 3) the changing spectral characteristics of the normalized waveforms to better understand the relative proportion of fracturing vs. fluid / magma movement [e.g., Burlini et al., 2007; Benson et al., 2008]. Whilst all these methods have proven useful in situations that have resulted in eruption, such as the 1991 eruption of Mt. Pinatubo [Mori et al., 1996] and the eruptive period between 2004 and 2008 at Mt. St. Helens [Kendrick et al., 2012], a great many cases exist where increasing seismic event rates have not resulted in eruption. This is often attributed to magma, in the form of dykes, stalling at depth [De Natale et al., 1997]. This is supported by field observations of arrested dykes [e.g., Gudmundsson, 2003], and recent research that has focused on the mechanics of dyke arrest [e.g., Gudmundsson and Brenner, 2004; Gudmundsson, 2011] due to Cook-Gordon delamination, stress barriers, and elastic mismatch. However, these ‘false alarms’ remain poorly understood. While there are plenty of examples where seismicity is correlated to movement of dykes through the country rock [e.g., Gudmundsson et al., 2014; Browning and Gudmundsson, 2015; Sigmundsson et al., 2015], it remains unclear how this movement results in the seismicity that is recorded at the surface.

To investigate some of these dyke intrusion and propagation processes, previous laboratory work has employed analogue materials such as dyed water or glycerin injected into a second medium [e.g., Taisne and Tait, 2011]. Such analogue studies have proven extremely useful,
but are so far restricted to room pressure/temperature and cannot record any seismicity generated at the moving dyke tip. In contrast, laboratory rock deformation studies of volcano processes employing acoustic emission (AE) as proxy for tectonic earthquakes [Kilburn, 2012], has produced data that is qualitatively similar to many types of volcano-seismic signals, yet is largely restricted to deformation in the compressional regime. Moreover, the use of AE is restricted to modest temperatures due to the temperature limits of the sensors (ca. 200 °C, Benson et al., 2010]. To date the investigation of rock fracture in tension due to an over-pressurized (dyke-like) conduit at *in-situ* temperatures [Benson et al., 2012] have employed only 2 AE sensors, located remotely and connected to the ‘hot zone’ via waveguides. We know that the use of multiple AE sensors is a potentially very powerful tool to examine such processes on a small scale, particularly in terms of spatio-temporal frequency analysis [e.g., Burlini et al., 2007]. Therefore, in this study we investigate the process of dyking in volcanic edifices by using an optimized hybrid composed of elements of both of the above techniques. Below we describe the initial results of a technique that operates at elevated temperatures using an analogue material, but with an array of AE sensors so that the dyke initiation and movement may be analyzed.

It has been well established that dykes form in two stages: (1), the rapid initiation and opening of a mode 1 fracture, followed by (2), the infill of that fracture by a fluid. If the fluid is sufficiently pressurized, it exerts that pressure on the walls of the fracture, causing the fracture tip to propagate [e.g., Brenner and Gudmundsson, 2004]. Thus, dyking is a key magma transport process especially during the approach of magma to the surface. Both stages are likely to be seismogenic, and that seismicity can be used to infer processes at depth in sub-volcanic systems. Here we report the results of experiments including both stages, including the seismic characteristics of dyke injection process at elevated pressure and temperature (PT) conditions.
2. Methods

Our experiments employ a standard triaxial apparatus modified to incorporate an internal sample assembly (Fig. 1) which has been designed to apply a tensile stress to the inner surface of a conduit or “borehole” as described by Benson et al. (2012). This set-up is similar to that of classic hydraulic fracturing studies [e.g., Hoskins, 1969; Santarelli and Brown, 1989; Vinciguerra et al., 2004] with two important exceptions: (1) in the materials types; and (2) the lack of inner wall jacket. In our experiments the pressurizing medium is a rod of Poly(Methyl Methacryllate (PMMA or ‘Plexiglas’) a viscoelastic material that is molten at the temperature of the experiment (175 °C). PMMA is ideal for our purpose as its glass transition temperature \(T_g\) occurs at a temperature of ca. 100 °C (depending on composition), and behaves as a liquid when used at temperatures above \(T_g\) and appropriate timescales. Further, its Newtonian viscosity-temperature relationship is well-known (~10^5 Pa.s. at 175 °C, see Hieber and Chiang, 1992). The permeability of the host rock is sufficiently low that PMMA seepage through the host rock has an insignificant effect on the timescale of the experiment [Etna basalt, Fortin et al., 2011; Comiso limestone, Bakker et al., 2015]. The use of PMMA at elevated temperatures has the benefit that the PMMA volume entering the fracture will solidify when the temperature falls below \(T_g\), thereby preserving the geometry of the fracture for later characterization. Unlike earlier work [e.g., Benson et al., 2012], the new apparatus is able to apply a confining pressure (oil) to simulate modest burial depths, as well as using a 12 piezoelectric sensor array, made possible due to the lower temperatures imposed.

Our initial experiments employed samples of basalts obtained from lava flows on Mt. Etna. We chose this rock type as it is considered a representative volcanic rock in a wide range of investigations, including seismic velocities [Vinciguerra et al., 2005] cyclic loading experiments in compression [Heap et al., 2009] and tension [Benson et al., 2012]. Recent work at elevated temperatures (Bakker et al., manuscript in preparation, 2015) has found that
Etna basalt does not show a deviation in mechanical behavior until the temperature exceeds 700 °C. Although these tests were performed in compression (at 50 MPa of confinement), we assume that this is also true in tension, allowing us to interpret the results over a wide range of temperature conditions.

Samples were co-axially drilled using a dual diamond drill bit so as to ensure a constant wall thickness. Samples were cut to 72 mm length, with an outer diameter of 40 mm and a 15 mm bore, resulting in a 12.5 mm wall thickness. The bore was filled with a 15 mm diameter PMMA rod, of approximately 55 mm length. The top and bottom parts of the inner hole were sealed using steel plugs, fitted with high-temperature resistant O-rings. In order to impose a stress on the PMMA rod, and thus pressurize the inner wall of the rock, the top plug is free to move into the sample bore through a central hole in the assembly. To allow movement, the space between the piston and rock sample is left open to the confining pressure. This provides a compensating pressure on the piston, as well as an axial stress on the sample (equal to the radial stress, see Fig. 1). The entire setup is jacketed using an engineered nitrile jacket made from high temperature rubber, that includes 12 ports for AE sensors.

The sample assembly is installed in a conventional triaxial compression apparatus capable of confining pressures of 100 MPa and fitted with an external furnace capable of reaching 200°C. Confining pressure and axial load are servo-controlled by two screw jack volumeters. AE are recorded on an array of 12 piezoelectric sensors, with signals pre-amplified by 60 dB prior to being split between two separate recording systems. The first system operates in “triggered” mode whereby discrete waveforms are recorded whenever any one of the 12 channels exceeds a pre-determined voltage threshold. The second system records the waveform continuously to high-speed hard disk storage. Both systems digitize the signals at 10 MHz and at 16-bit resolution. Post-test, an automated picking routine (ITASCA-IMAGE “InSite” seismic processor) was used to obtain P-wave arrivals for each sensor that
were manually checked and corrected when necessary. In order to avoid refracted and reflected waves from the rock-PMMA interface, we chose to only locate the events using the sensors with the lowest arrival times, from the half of the array nearest the generated fracture, as it is likely that these waves have only travelled directly through the rock from event location to sensor, and are not refracted or reflected.

Using the above method and protocols, we have investigated two inter-related scenarios: (1) the increase of a conduit overpressure (compared to confinement pressure) with constant confinement pressure in which a new fracture (dyke) is generated, and (2) the character of the continuous AE recorded once the fracture and dyke has formed. A confining pressure of 30 MPa was applied, simulating a depth of approximately 1.5 km, and a constant displacement rate for the top piston movement of 1 µm/s was used. In both cases a basic AE location, using the radial statistics of event direction frequency as taken from the relevant aspect of the array (avoiding path/interface effects), is mapped and compared to the pressures required to open and sustain the fracture. After each test the samples were returned to a hydrostatic stress state before cooling down to room temperature.
3. Results

Figure 2 shows 1) the conduit overpressure and 2) the AE hit rate as a function of time for the Etna basalt (Fig. 2A) at 175 °C. The conduit pressure rises quickly in the first 150 seconds as initial pressurization of the molten PMMA occurs, after which the AE hit rate becomes measurable. After ca. 800 seconds a clear increase in AE hit rate coincides with a slowing conduit pressurization rate. Pressurization continues to a calculated peak-overpressure of 12 MPa at which point a spike in AE is recorded and a fall in conduit pressure. This is likely to represent the initial fracture. Continued movement of the pressuring piston did not yield any further increase in conduit pressure, and AE hit rate falls at approximately 1400 seconds to pre-fracture levels, with minor peaks associated with stress drops in the order of 1 MPa. At 2750 seconds the conduit stressed was released (to hydrostatic conditions) and experiment was concluded. AE location data from the experiment (Fig. 2B) indicated that two fractures formed at 180° with a well-clustered center. Importantly, these data agree well with post-test visual inspection (Fig. 2C).

Our further experiments employed Comiso limestone (Fig. 3) also at 175 °C. They show a generally similar pattern. Conduit pressurization is initially slower, reaching a peak of approximately 7.2 MPa at 1000 seconds. The onset of AE occurs very rapidly, at 700 seconds, with a peak AE hit rate of only 5 hits per 10 seconds (compared to a maximum hit rate in the Etna basalt experiment of over 300 hits per 10 seconds). A clear break in slope in the conduit pressurization curve is seen at 800 seconds. However, continued pressurization likely results in failure at 1000 seconds at which time a second spike in AE hit rate is also recorded. After this time, the conduit pressure decreases, and AE activity rapidly subsides. At 2100 seconds the piston advance is stopped and the PMMA is allowed to relax, a process which is accompanied by minor AE. At 3000 seconds the conduit stressed is released and the experiment is terminated. Data from radial AE location (Fig. 3B) is relatively poorly-focused.
but nevertheless contains indications of radial fracture at 45°, 120°, 235° and 300° (Fig. 3C).

These orientations generally match visual characterization of the fractures from post-experiment imaging in all but the 45° direction. In addition, considerably fewer AE hits were recorded, (i.e., < 10 events per sector). Due to these limitations, and the fact that this unit is found deeper in the Etnan basement (likely at temperatures beyond the brittle to ductile transition, see Bakker et al., 2015) we applied our main focus below to the basalt experiments, including the analysis of the generated AE and post-test samples.

Spectral analysis of the AE data is shown in figure 4. The examples of waveform data shown are (indicated by arrows on Fig. 2A), were obtained during the main fracturing event and the PMMA movement, respectively. The waveform taken at 900 seconds (fracture) illustrates many of the classical features of an impulsive AE event with a rapid onset, short coda, and significant power across a broad frequency band to approximately 600 kHz (Fig. 4A).

Conversely, the example of waveform data from the post-fracture segment at 1400 seconds (Fig. 4B) shows a very different character. Typical waveforms have a highly emergent nature, with a protracted coda exhibiting the type of ringing or resonance frequently seen during harmonic tremor seismic activity. The spectrogram analysis is consistent with this character (Fig. 4B) illustrating a relatively monochromatic power spectrum centered at approximately 150 kHz and little power at frequencies over 250 kHz.

Post-test examination of the Etna samples illustrates the close match between fracture sets and AE data, with 2 fractures generated in the Etna sample. The PMMA has clearly intruded into the opened fracture, preserving the analogue dyke in-situ after the sample has quenched, as designed. This is illustrated in a montage of X-ray Computed Tomography images (Fig S1, and movies S1 to S3 also presented in supplementary material).
Formation of an extensional fracture is the first stage in dyke propagation, requiring the pressurizing fluid (here magma) to overcome the tensile strength of the country rock in a mode 1 fracture, and then to propagate as a feeder dyke [e.g., Gudmundsson, 2002]. Such features thus occur in both natural systems as well as hydrocarbon extraction technologies such as shale gas hydraulic fracturing [Rivalta et al., 2015]. Despite their importance, the precise pressures required for this mechanism to operate are poorly known. This is especially true for magmatic systems. Here a viscoelastic analogue “magma” (PMMA) has been used to generate thin dyke-like structures in both a classically “brittle” material (represented by the basalt) and a slightly more ductile unit (represented by the Comiso limestone) both of which occur as rock types in sub-volcanic basement and edifice. Both of these materials are well-studied in the rock mechanics and rock physics literature [e.g., Heap et al., 2009; Bakker et al., 2015]. In the case of the basalt, a clear and obvious fracture set is propagated when internal pressure exceeds 12 MPa. This is in general agreement with previous work at magmatic temperatures [Benson et al., 2012], where a conduit pressure of 15 MPa was required at a temperature of 918 °C. A key advantage of the current experimental adaptation lies in the more advanced AE setup with which to chart the AE preferential directions (via a statistical approach) and to analyze the character of the recorded waveforms. It is this tool that reveals key differences between the emitted AE, and by extension field seismicity, during the different phases of dyke generation, which relies primarily on a mechanical generation, and the movement of the viscous “magma” through the fracture.
The magnitude and number of AE recorded are significantly greater in the basalt experiment. This likely results from the greater strength of the basalt with respect to the limestone, whereby fracturing is associated with larger stress releases than those responsible for the AE generated by fracturing of limestone. It is, indeed a well-known observation that calcite-rich rocks produce fewer AE than most rocks with other mineral composition [e.g., Cartwright-Taylor et al., 2014]. This behavior is reflected in both the statistics of the recorded AE, as well as the location of those AE around the sample.

As demonstrated in previous work at much higher temperatures [Benson et al., 2012], and in both cases, the recorded AE serve as a useful proxy for determining when the sample fails. This consistency of old and new results confirms the utility of the use of a lower temperature analogue at 175 °C, with similar injected structures observed (Fig. S1), and similar pressures required to promote the initial mode 1 failure.

A major area of current research in volcanic active areas is the occurrence of intense seismicity which is not followed immediately by eruption. Such ‘seismic crises’ cause significant alarm to the local authorities and population and have occurred in densely populated areas such as the Campi Flegrei caldera around the city of Naples, Italy [D’Auria et al., 2015]. Recent work has suggested that fluid migration plays a significant role in the local deformation (uplift) as well as the seismicity [e.g., De Natale et al., 1997; Battaglia et al., 2006] and the debate on the relative roles of hydrothermal and magmatic contributions to unrest events in this area continue to this day. Here, we observe that after the initial fracturing (analogous to dyke emplacement) not only the AE rate subsides (despite constant deformation/fluid injection rates) but also the conduit pressure continues to decrease. We link the reduction in AE in the experiments to the deflating caldera in nature and suggest that as magma stalls within newly established dykes at depth a decrease in pressure occurs (assuming that inflow from deeper reservoirs is significantly slower than outflow through the dyke), as
observed in our experiments. This is matched by a concomitant decrease in seismic event rates, also observed in our experiments, although it is noted that the rate does not fall off completely, unlike field seismic data as described in Browning and Gudmundsson [2015]. Finally, we note that the character of the AE changes significantly before and after fracturing (dyke) formation from the characteristic high frequency of brittle fracture to something resembling a resonance that is often taken as an indicator of fluid movement [e.g., Chouet, 1996], further supporting the idea that the established conduit is influencing the character of seismicity generated in such regions and that magma movement may be at the source of it all.

5. Summary

We have developed a method for investigating dyke injection in a controlled pressure and temperature environment using PMMA as an analogue injection material of high viscosity with which to pressurize an inner bore of a specimen material in tension, and thus form and propagate a dyke. By using an array of AE sensors mounted around the specimen, we have compared and contrasted the seismic waveforms generated during the fracture event, and during fluid flow after the fracture was formed. We conclude that the movement of this viscous fluid has the potential to generate low frequency harmonic tremor similar to that observed in field-scale volcanic processes. We measure an overpressure (of the PMMA compared to confining pressure) required to initially form a dyke of around 12 MPa in basalt when confined at 30 MPa. These results are similar to previous studies, in that a lower pressure is then needed to continue dyke propagation. In both cases, a significant AE, analogous to field seismicity is measured. We further conclude that the generation and stalling of magmatic dykes in shallow caldera systems is a likely source for much of the seismicity of such regions, as well as explaining some of the characteristic inflation and deflation.
6. Acknowledgements

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Figures

Figure 1
Figure 4
Figure Captions

Figure 1: Simplified schematic (cross section) of the sample assembly which sits inside the triaxial pressure vessel. In this setup, the top piston (normally providing an axial principal stress, $\sigma_1$) is used to apply a stress to the top area of a molten PMMA plug that expands laterally, pressurizing the entire conduit and applying a tensile stress to the inner surface of the wall rock (Etna basalt). The system is encapsulated by a rubber jacket embedded with 12 AE sensors for the detection of Acoustic Emission (AE), as well as a steel lower and floating, sealed, top annulus.

Figure 2: (A), Radial pressurization of Etna basalt at 175 °C peaks at a conduit pressure of 12 MPa, coinciding with a peak in Acoustic Emission hit rate of approximately 335 hits per 10 second interval, after which point the conduit pressure falls, suggesting fracture of the wall rock. AE location (B) of the AE radial position suggests two dominant fracture positions, which is in agreement with post-test examination (C) of the sample.

Figure 3: (A), Radial pressurization of Comiso limestone at 175 °C peaks at a lower pressure of 7.2 MPa with a longer build-up. AE is lower than the equivalent data for the basalt, with two spikes in AE rate of approximately 11 and 18 hits per 10 second interval. The former of these AE peaks coincides with a break in conduit pressure increase followed by prominent decrease in pressure, interpreted as the failure of outer shall. Radial AE location (B) exhibits a wide range of fracture orientations, with three of these directions agreeing with post-test inspection of the sample (C).
Figure 4: (A) Events during the initial fracture of the Etna basalt shell (arrow in Fig. 2, approximately 900 seconds) show numerous features of the classical volcano-tectonic waveform such as a sharp onset. In contrast waveforms collected after the pressure drop at approximately 1400 seconds (B), after fracture formation and during ingress of molten PMMA into the generated fracture, exhibits features of so-called low frequency (LF) type events such as a long coda and resonant or ‘ringing’ nature. Spectrograms of the waveforms support this interpretation, showing polychromatic features characteristic of volcano tectonic (VT)-type waveforms during fracture (C), where power is spread between 10 kHz (hardware filter minimum) through to approximately 600 kHz. In contrast LF-type waveforms (D) collected during PMMA ingress have monochromatic features with the majority of spectral power centered around 150 kHz.

References


Brenner, S. L., and a. Gudmundsson (2004), Arrest and aperture variation of hydrofractures


Heap, M. J., S. Vinciguerra, and P. G. Meredith (2009), The evolution of elastic moduli with
increasing crack damage during cyclic stressing of a basalt from Mt. Etna volcano,


Vinciguerra, S., P. G. Meredith, and J. Hazzard (2004), Experimental and modeling study of